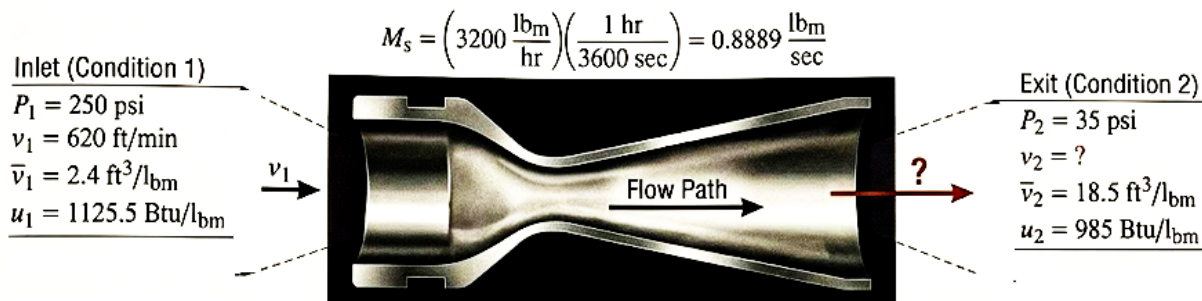


An engineering device designed to vary the velocity of a moving fluid by modifying its cross-sectional passage area is classified as a **Nozzle**.



In a fluid system running under stable operating parameters, a nozzle represents an **Open System** governed by **The First Law of Thermodynamics for Steady Flow**. Because a nozzle's primary task is to convert thermal energy directly into directed macroscopic movement, several unique operating parameters apply:

- **Adiabatic Operation ($Q = 0$):** The velocity of the fluid stream passing through a nozzle is so high that the substance spends a negligible fraction of a second inside the device. Consequently, there is virtually no time for heat to transfer across the solid perimeter walls to or from the external room environment ($q = 0$).
- **No Shaft Work Output ($W_{sf} = 0$):** Unlike a steam turbine or reciprocating piston assembly, a nozzle features absolutely no moving internal parts, rotating blades, or linkages. It cannot capture or generate mechanical shaft power ($w_{sf} = 0$).
- **Negligible Potential Energy Changes ($\Delta PE = 0$):** The structural alignment of a standard nozzle is horizontal, and any small elevation differences between the inlet and outlet centerlines produce a mathematically insignificant hydrostatic impact.

Given these constraints, the standard **Steady-Flow Energy Equation (SFEE)** on a per-unit-mass basis (1 lb_m) simplifies to a strict balance between entering Enthalpy ($h_1 = u_1 + P_1 V_1$) and Kinetic Energy (KE_1) versus exiting Enthalpy ($h_2 = u_2 + P_2 V_2$) and Kinetic Energy (KE_2):

$$U_1 + P_1 \bar{v}_1 + \frac{v_1^2}{2g_c} = U_2 + P_2 \bar{v}_2 + \frac{v_2^2}{2g_c}$$

Rearranging this expression to solve for the structural change in kinetic energy yields:

$$\Delta KE = \frac{v_2^2 - v_1^2}{2g_c} = - \left(U_2 - U_1 \right) - \left(P_2 \bar{v}_2 - P_1 \bar{v}_1 \right)$$

Where $g_c = 32.2 \frac{\text{lb}_m \cdot \text{ft}}{\text{lb}_f \cdot \text{sec}^2}$ is the universal gravitational proportional conversion factor for the United States Customary System (USCS), which is vital to balance mechanical force and thermal components safely.

Step 1: Extract and Standardize Input Data

- Mass Flow Rate ($\dot{m}$) = 3200 lb_m/hr (This value is actually redundant since the calculation can be solved purely on a per-unit-mass basis)
- Inlet Pressure (P_1) = 250 psi = 250 lb_f/in²
- Inlet Velocity (v_1) = 620 ft/min = $\frac{620}{60} \frac{ft}{sec} = 10.3333 \text{ ft/sec}$
- Inlet Specific Volume ($\bar{v}_1$) = 2.4 ft³/lb_m
- Inlet Internal Energy (U_1) = 1125.5 Btu/lb_m
- Outlet Pressure (P_2) = 35 psi = 35 lb_f/in²
- Outlet Specific Volume ($\bar{v}_2$) = 18.5 ft³/lb_m
- Outlet Internal Energy (U_2) = 985 Btu/lb_m

Step 2: Calculate Specific Internal Energy Change (ΔU)

$$\Delta U = (U_2 - U_1) = (985 - 1125.5) = -140.5 \frac{\text{Btu}}{\text{lb}_m}$$

Step 3: Calculate Specific Flow Work Change (ΔW_f)

$$\Delta W_f = \left(P_2 \bar{v}_2 - P_1 \bar{v}_1 \right) = \left(35 \frac{\text{lb}}{\text{in}^2} \right) \left(\frac{144 \text{ in}^2}{1 \text{ ft}^2} \right) \left(18.5 \frac{\text{ft}^3}{\text{lb}_m} \right) - \left(250 \frac{\text{lb}}{\text{in}^2} \right) \left(\frac{144 \text{ in}^2}{1 \text{ ft}^2} \right) \left(2.4 \frac{\text{ft}^3}{\text{lb}_m} \right)$$

$$\Delta W_f = \left(6840 \frac{\text{lb}_f \text{ ft}}{\text{lb}_m} \right) \left(\frac{1 \text{ Btu}}{778 \text{ lb}_f \text{ ft}} \right) = 8.7918 \frac{\text{Btu}}{\text{lb}_m}$$

Step 4: Combine the Enthalpy Component Drop

Using the values derived above, find the total change in specific kinetic energy (ΔKE):

$$\Delta KE = -\Delta U - \Delta W_f = - \left(-140.5 \frac{\text{Btu}}{\text{lb}_m} \right) - \left(8.7918 \frac{\text{Btu}}{\text{lb}_m} \right) = 131.7101 \frac{\text{Btu}}{\text{lb}_m}$$

$$\Delta KE = \left(131.7101 \frac{\text{Btu}}{\text{lb}_m} \right) \left(\frac{778 \text{ lb}_f \text{ ft}}{1 \text{ Btu}} \right) = 102,492.684 \frac{\text{lb}_f \text{ ft}}{\text{lb}_m}$$

Since $\Delta KE = \frac{v_2^2 - v_1^2}{2g_c}$,

$$102,492.684 \frac{\text{lb}_f \text{ ft}}{\text{lb}_m} = \frac{v_2^2 - v_1^2}{2 \left(\frac{\text{lb}_m \text{ ft}}{\text{lb}_f \text{ sec}^2} \right)}$$

$$v_2^2 - v_1^2 = 6,595,093.243 \frac{\text{ft}^2}{\text{sec}^2}$$

Step 5: Solve for Final Exit Velocity (v_2)

$$v_2^2 - \left(10.3333 \frac{ft}{sec}\right)^2 = 6,595,093.243 \frac{ft^2}{sec^2}$$

$$v_2 = 2,568.11 \frac{ft}{sec}$$

In power generation plants, this high-speed jet leaving a nozzle array is immediately slammed against the curved blades of a steam turbine rotor. The massive momentum change of the fluid jet creates a high hydrodynamic torque profile, spinning large electrical generators. Accurate nozzle calculations are mandatory to optimize kinetic transfer efficiency and protect turbine structural limits against supersonic shockwave erosion.